

# OPTIMAL DESIGN OF STRUCTURES (MAP 562)

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CHAPTER VII

TOPOLOGY OPTIMIZATION

BY THE HOMOGENIZATION METHOD

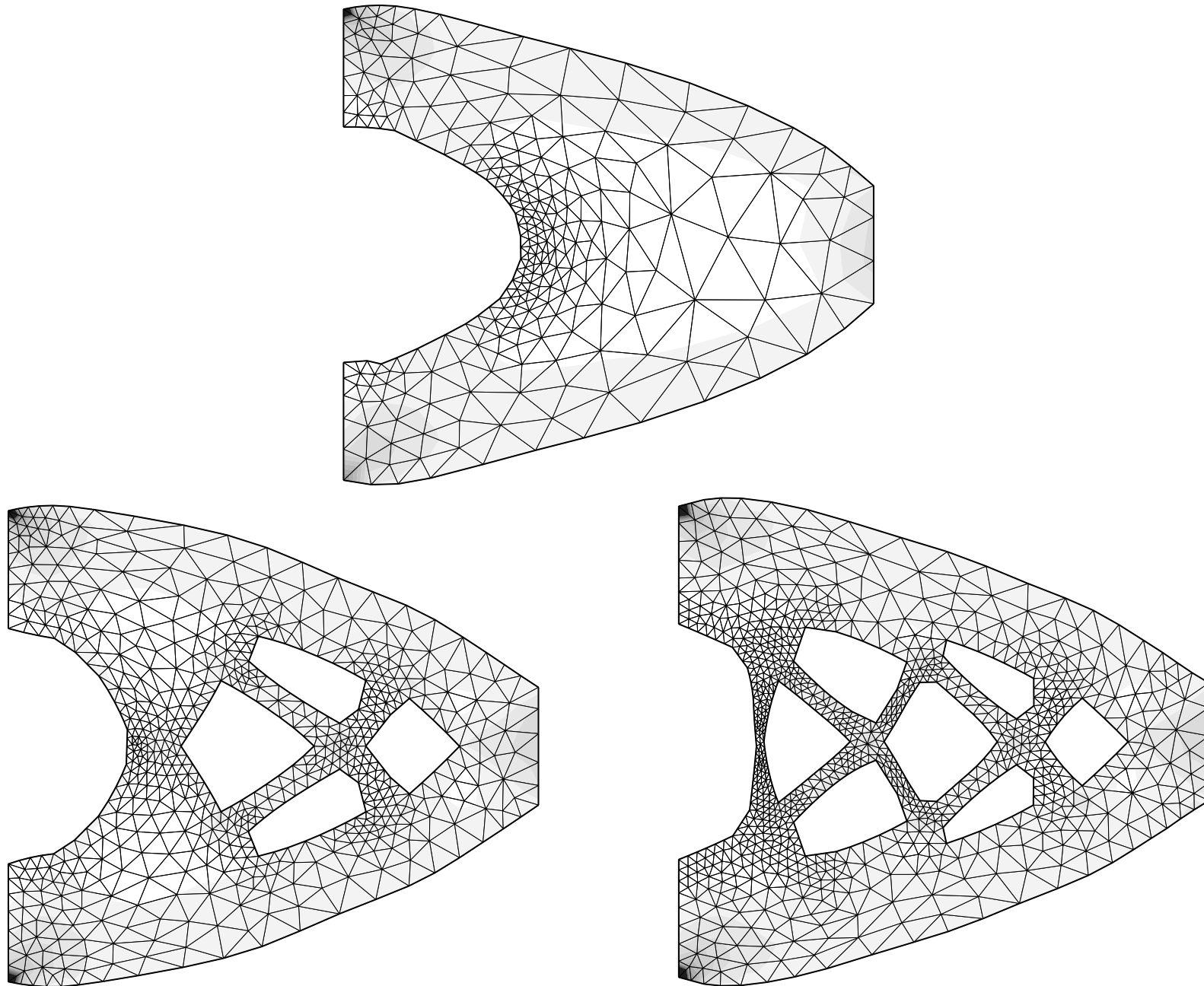
## Why topology optimization ?

### Drawbacks of geometric optimization:

- ➡ no variation of the **topology** (number of holes in 2-d),
- ➡ many local minima,
- ➡ CPU cost of remeshing (mostly in 3-d),
- ➡ **ill-posed** problem: non-existence of optimal solutions (**in the absence of constraints**). It shows up in numerics !

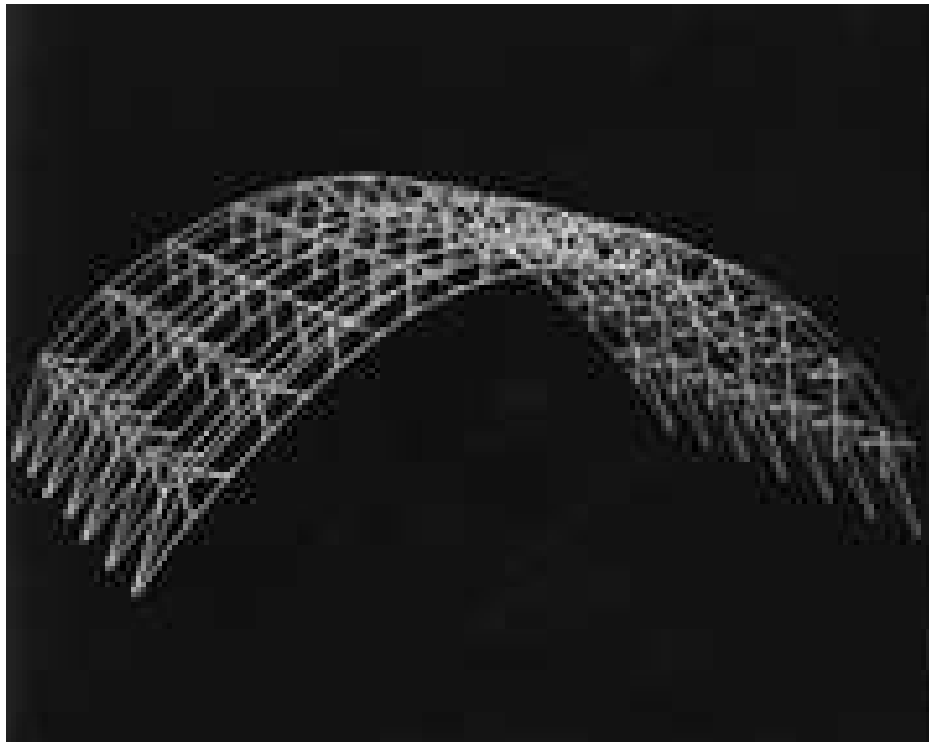
**Topology optimization:** we improve not only the boundary location but also its topology (**i.e., its number of connected components in 2-d**).

We focus on one possible method, **based on homogenization**.



The art of structure is where to put the holes.

Robert Le Ricolais, architect and engineer, 1894-1977



## Principles of the homogenization method

The homogenization method is based on the concept of “relaxation”: it makes ill-posed problems well-posed by enlarging the space of admissible shapes.

We introduce “generalized” shapes but not too generalized... We require the generalized shapes to be “limits” of minimizing sequences of classical shapes.

**Remember the counter-example of Section 6.2.1:** the minimizing sequences of shapes had a tendency to build **fine mixtures of material and void**.

Homogenization allows as admissible shapes **composite materials** obtained by microperforation of the original material.

## Notations

⇒ A **classical shape** is parametrized by a characteristic function

$$\chi(x) = \begin{cases} 1 & \text{inside the shape,} \\ 0 & \text{inside the holes.} \end{cases}$$

⇒ From now on, the holes can be microscopic as well as macroscopic  $\Rightarrow$  porous composite materials !

⇒ We parametrize a **generalized shape** by a **material density**  $\theta(x) \in [0, 1]$ , and a **microstructure (or holes shape)**.

⇒ The holes shape is very important ! It induces a new optimization variable which is the **effective behavior**  $A^*(x)$  of the composite material (defined by homogenization theory).

⇒  $(\theta, A^*)$  are the two new optimization variables.

### 7.1.2 Model problem

**Simplifying assumption:** the “holes” with a free boundary condition (Neumann) are filled with a **weak (“ersatz”) material**  $\alpha \ll \beta$ .

**Membrane with two possible thicknesses**  $h_\chi(x) = \alpha\chi(x) + \beta(1 - \chi(x))$ , with

$$\mathcal{U}_{ad} = \left\{ \chi \in L^\infty(\Omega; \{0, 1\}), \int_\Omega \chi(x) dx = V_\alpha \right\}.$$

If  $f \in L^2(\Omega)$  is the applied load, the displacement satisfies

$$\begin{cases} -\operatorname{div}(h_\chi \nabla u_\chi) = f & \text{in } \Omega \\ u_\chi = 0 & \text{on } \partial\Omega. \end{cases}$$

Optimizing the membrane’s shape amounts to minimize

$$\inf_{\chi \in \mathcal{U}_{ad}} J(\chi),$$

with

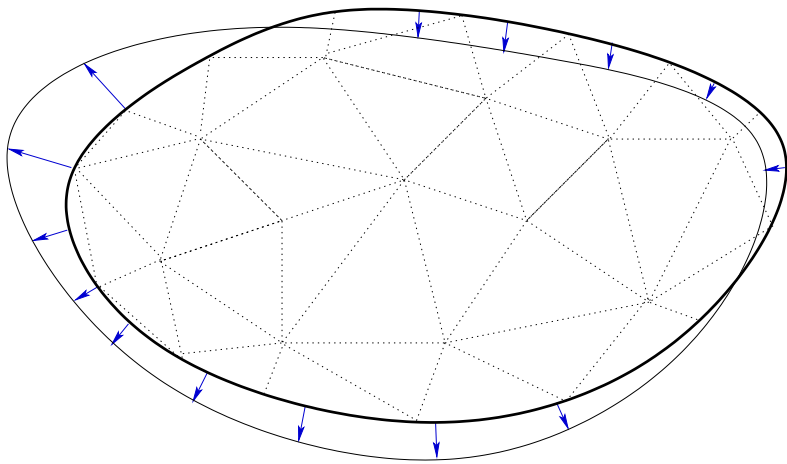
$$J(\chi) = \int_\Omega f u_\chi dx, \quad \text{or} \quad J(\chi) = \int_\Omega |u_\chi - u_0|^2 dx.$$

## Goals of the homogenization method

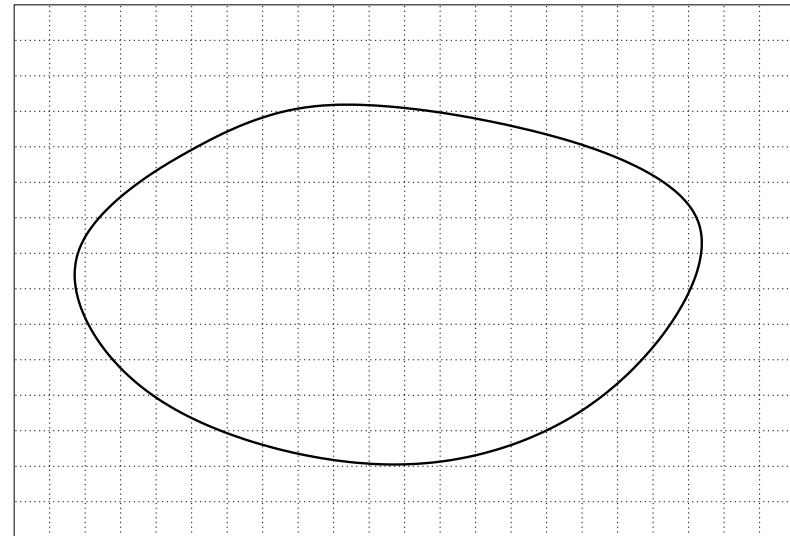
- ➡ To introduce the notion of generalized shapes made of **composite material**.
- ➡ To show that those generalized shapes are limits of sequences of classical shapes (in a sense to be made precise).
- ➡ To compute the generalized objective function and its gradient.
- ➡ To prove an existence theorem of optimal generalized shapes (it is **not** the goal of the present course).
- ➡ To deduce **new numerical algorithms** for topology optimization (it is **actually** the goal of the present course).

While geometric optimization was producing **shape tracking** algorithms, topology optimization yields **shape capturing** algorithms.



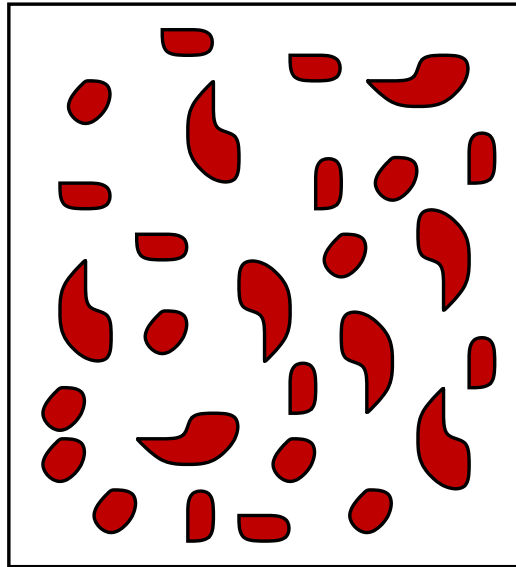


Shape tracking

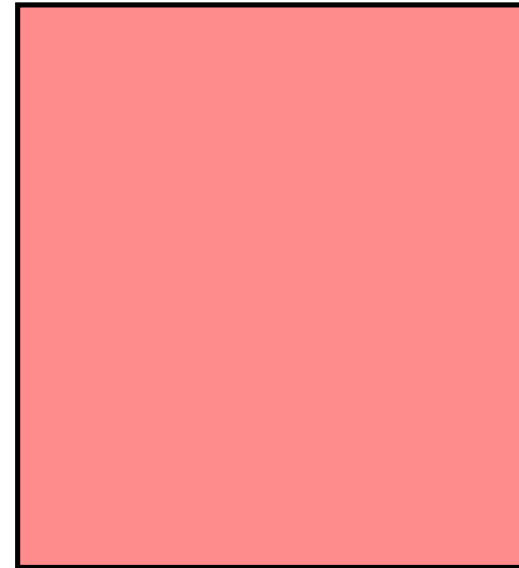


Shape capturing

## 7.2 Homogenization



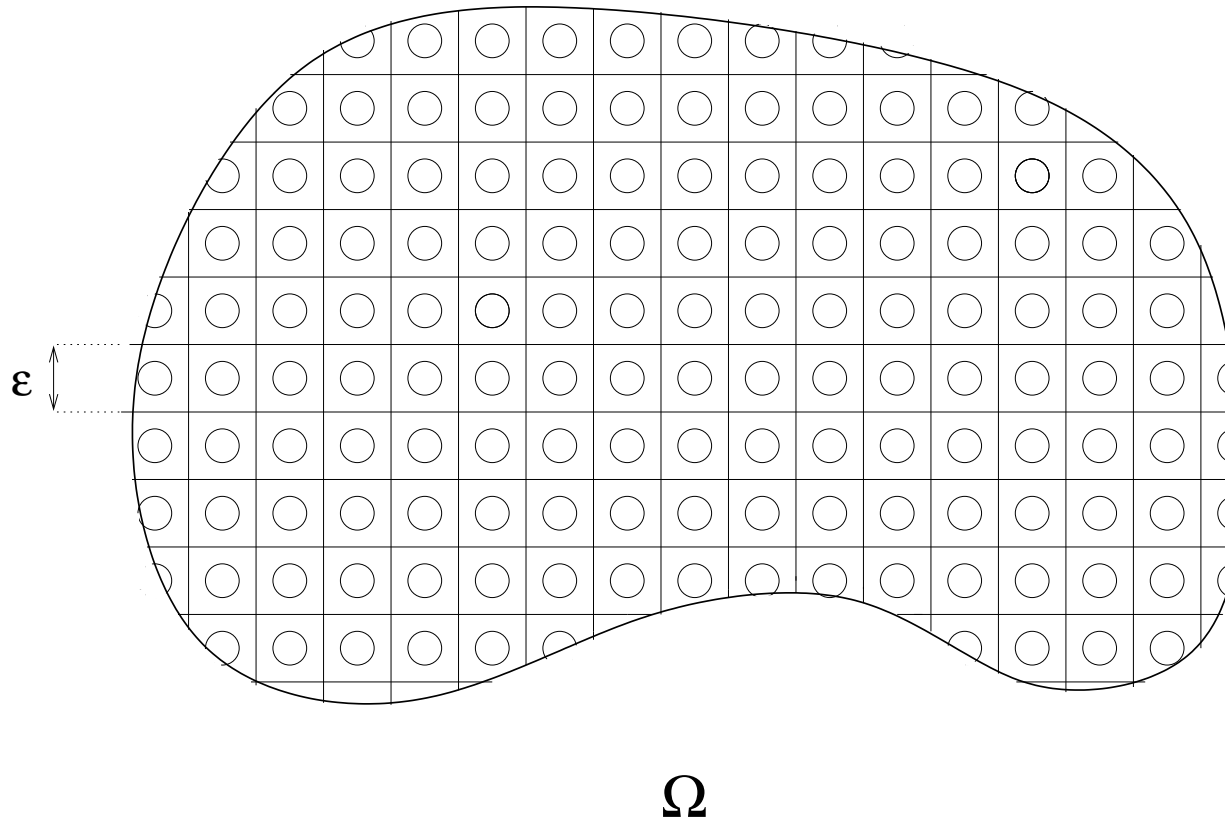
**MILIEU HETEROGENE**



**MILIEU EFFECTIF  
(MATERIAU COMPOSITE)**

- ⇒ Averaging method for partial differential equations.
- ⇒ Determination of averaged parameters (or effective, or homogenized, or equivalent, or macroscopic) for an heterogeneous medium.

## Periodic homogenization



Different approaches are possible: we describe the simplest one, i.e., [periodic homogenization](#).

**Assumption:** we consider [periodic](#) heterogeneous media.

## Periodic homogenization (Ctd.)

- ➡ Ratio of the period with the characteristic size of the structure =  $\epsilon$ .
- ➡ Although, for the “true” problem under consideration, there is only one physical value  $\epsilon_0$  of the parameter  $\epsilon$ , we consider a **sequence of problems** with smaller and smaller  $\epsilon$ .
- ➡ We perform an **asymptotic analysis** as  $\epsilon$  goes to 0.
- ➡ We shall approximate the “true” problem ( $\epsilon = \epsilon_0$ ) by the limit problem obtained as  $\epsilon \rightarrow 0$ .

**Model problem: elastic membrane made of composite material**

For example: periodically distributed fibers in an epoxy resin.

**Variable Hooke's law:**  $A(y)$ ,  $Y$ -periodic function, with  $Y = (0, 1)^N$ .

$$A(y + e_i) = A(y) \quad \forall e_i \text{ } i\text{-th vector of the canonical basis.}$$

We replace  $y$  by  $\frac{x}{\epsilon}$ :

$$x \rightarrow A\left(\frac{x}{\epsilon}\right) \text{ periodic of period } \epsilon \text{ in all axis directions.}$$

Bounded domain  $\Omega$ , load  $f(x)$ , displacement  $u_\epsilon(x)$  solution of

$$\begin{cases} -\operatorname{div}\left(A\left(\frac{x}{\epsilon}\right)\nabla u_\epsilon\right) = f & \text{in } \Omega \\ u_\epsilon = 0 & \text{on } \partial\Omega, \end{cases}$$

A direct computation of  $u_\epsilon$  can be very expensive (since the mesh size  $h$  should satisfy  $h < \epsilon$ ), thus we seek only the **averaged values** of  $u_\epsilon$ .

## Two-scale asymptotic expansions

We assume that

$$u_\epsilon(x) = \sum_{i=0}^{+\infty} \epsilon^i u_i \left( x, \frac{x}{\epsilon} \right),$$

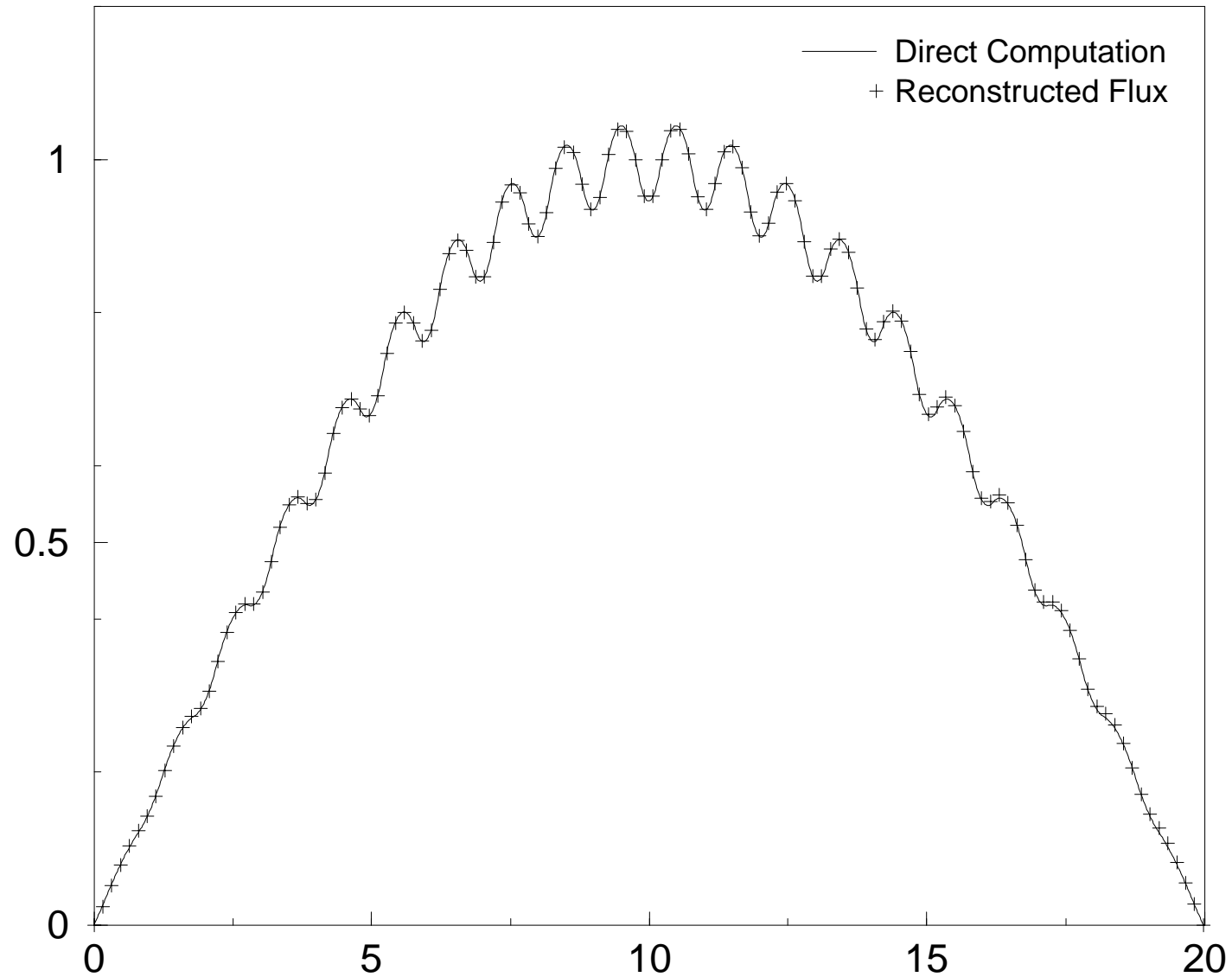
with  $u_i(x, y)$  function of the two variables  $x$  and  $y$ , **periodic in  $y$**  of period  $Y = (0, 1)^N$ . Plugging this series in the equation, we use the derivation rule

$$\nabla \left( u_i \left( x, \frac{x}{\epsilon} \right) \right) = \left( \epsilon^{-1} \nabla_y u_i + \nabla_x u_i \right) \left( x, \frac{x}{\epsilon} \right).$$

Thus

$$\nabla u_\epsilon(x) = \epsilon^{-1} \nabla_y u_0 \left( x, \frac{x}{\epsilon} \right) + \sum_{i=0}^{+\infty} \epsilon^i \left( \nabla_y u_{i+1} + \nabla_x u_i \right) \left( x, \frac{x}{\epsilon} \right).$$

Typical oscillating behavior of  $x \rightarrow u_i(x, \frac{x}{\epsilon})$



The equation becomes a series in  $\epsilon$

$$\begin{aligned}
 & -\epsilon^{-2} \left[ \operatorname{div}_y (A \nabla_y u_0) \right] \left( x, \frac{x}{\epsilon} \right) \\
 & -\epsilon^{-1} \left[ \operatorname{div}_y (A (\nabla_x u_0 + \nabla_y u_1)) + \operatorname{div}_x (A \nabla_y u_0) \right] \left( x, \frac{x}{\epsilon} \right) \\
 & - \sum_{i=0}^{+\infty} \epsilon^i \left[ \operatorname{div}_x (A (\nabla_x u_i + \nabla_y u_{i+1})) + \operatorname{div}_y (A (\nabla_x u_{i+1} + \nabla_y u_{i+2})) \right] \left( x, \frac{x}{\epsilon} \right) \\
 & \qquad \qquad \qquad = f(x).
 \end{aligned}$$

- ☞ We identify each power of  $\epsilon$ .
- ☞ We notice that  $\phi \left( x, \frac{x}{\epsilon} \right) = 0 \quad \forall x, \epsilon \quad \Leftrightarrow \quad \phi(x, y) \equiv 0 \quad \forall x, y$ .
- ☞ Only the three first terms of the series really matter.

We start by a technical lemma.



**Lemma 7.4.** Take  $g \in L^2(Y)$ . The equation

$$\begin{cases} -\operatorname{div}_y (A(y)\nabla_y v(y)) = g(y) \text{ in } Y \\ y \rightarrow v(y) \text{ } Y\text{-periodic} \end{cases}$$

admits a unique solution  $v \in H_{\#}^1(Y)/\mathbb{R}$  if and only if

$$\int_Y g(y) dy = 0.$$

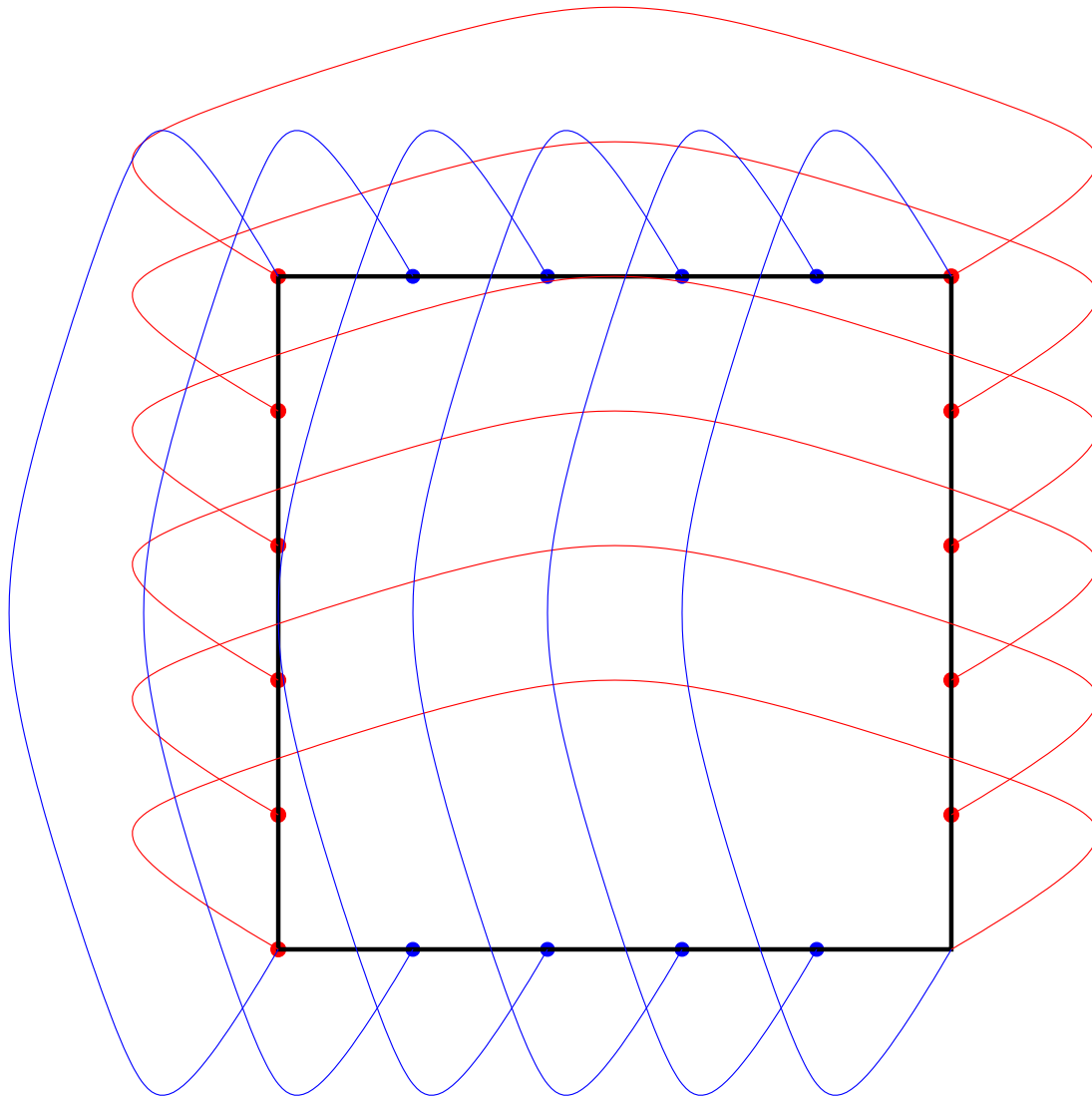
**Proof.** Let us check that it is a necessary condition for existence. Integrating the equation on  $Y$

$$\int_Y \operatorname{div}_y (A(y)\nabla_y v(y)) dy = \int_{\partial Y} A(y)\nabla_y v(y) \cdot n ds = 0$$

because of the **periodic boundary conditions**:  $A(y)\nabla_y v(y)$  is periodic but the normal  $n$  changes its sign on opposite faces of  $Y$ .

The sufficient condition is obtained by applying Lax-Milgram Theorem in  $H_{\#}^1(Y)/\mathbb{R}$ .

Periodic boundary conditions in  $H_{\#}^1(Y)$



Equation of order  $\epsilon^{-2}$ :

$$\begin{cases} -\operatorname{div}_y (A(y)\nabla_y u_0(x, y)) = 0 \text{ in } Y \\ y \rightarrow u_0(x, y) \text{ } Y\text{-periodic} \end{cases}$$

It is a p.d.e. with respect to  $y$  ( $x$  is just a parameter).

By uniqueness of the solution (up to an additive constant), we deduce

$$u_0(x, y) \equiv u(x)$$

Equation of order  $\epsilon^{-1}$ :

$$\begin{cases} -\operatorname{div}_y (A(y) \nabla_y u_1(x, y)) = \operatorname{div}_y (A(y) \nabla_x u(x)) & \text{in } Y \\ y \rightarrow u_1(x, y) & Y\text{-periodic} \end{cases}$$

The necessary and sufficient condition of existence is satisfied. Thus  $u_1$  depends linearly on  $\nabla_x u(x)$ .

We introduce the cell problems

$$\begin{cases} -\operatorname{div}_y (A(y) (e_i + \nabla_y w_i(y))) = 0 & \text{in } Y \\ y \rightarrow w_i(y) & Y\text{-periodic,} \end{cases}$$

with  $(e_i)_{1 \leq i \leq N}$ , the canonical basis of  $\mathbb{R}^N$ . Then

$$u_1(x, y) = \sum_{i=1}^N \frac{\partial u}{\partial x_i}(x) w_i(y)$$

Equation of order  $\epsilon^0$ :

$$\begin{cases} -\operatorname{div}_y (A(y)\nabla_y u_2(x, y)) = \operatorname{div}_y (A(y)\nabla_x u_1) \\ \quad + \operatorname{div}_x (A(y)(\nabla_y u_1 + \nabla_x u)) + f(x) \text{ in } Y \\ y \rightarrow u_2(x, y) \text{ Y-periodic} \end{cases}$$

The necessary and sufficient condition of existence of the solution  $u_2$  is:

$$\int_Y \left( \operatorname{div}_y (A(y)\nabla_x u_1) + \operatorname{div}_x (A(y)(\nabla_y u_1 + \nabla_x u)) + f(x) \right) dy = 0$$

We replace  $u_1$  by its value in terms of  $\nabla_x u(x)$

$$\operatorname{div}_x \int_Y A(y) \left( \sum_{i=1}^N \frac{\partial u}{\partial x_i}(x) \nabla_y w_i(y) + \nabla_x u(x) \right) dy + f(x) = 0$$

and we find the [homogenized problem](#)

$$\begin{cases} -\operatorname{div}_x (A^* \nabla_x u(x)) = f(x) \text{ in } \Omega \\ u = 0 \text{ on } \partial\Omega \end{cases}$$

## Homogenized tensor:

$$A_{ji}^* = \int_Y A(y) (e_i + \nabla_y w_i) \cdot e_j dy,$$

or, integrating by parts

$$A_{ji}^* = \int_Y A(y) (e_i + \nabla_y w_i(y)) \cdot (e_j + \nabla_y w_j(y)) dy.$$

Indeed, the cell problem yields

$$\int_Y A(y) (e_i + \nabla_y w_i(y)) \cdot \nabla_y w_j(y) dy = 0.$$

- ⇒ The formula for  $A^*$  is not fully explicit because cell problems must be solved.
- ⇒  $A^*$  does not depend on  $\Omega$ , nor  $f$ , nor the boundary conditions.
- ⇒ **The tensor  $A^*$  characterizes the microstructure.**
- ⇒ Later, we shall compute explicitly some examples of  $A^*$ .

One can prove:

$$u_\epsilon(x) = u(x) + \epsilon u_1\left(x, \frac{x}{\epsilon}\right) + r_\epsilon \quad \text{with} \quad \|r_\epsilon\|_{H^1(\Omega)} \leq C\epsilon^{1/2}$$

In particular

$$\|u_\epsilon - u\|_{L^2(\Omega)} \leq C\epsilon^{1/2}$$

The corrector is not negligible for the strain or the stress

$$\nabla u_\epsilon(x) = \nabla_x u(x) + (\nabla_y u_1)\left(x, \frac{x}{\epsilon}\right) + t_\epsilon \quad \text{with} \quad \|t_\epsilon\|_{L^2(\Omega)} \leq C\epsilon^{1/2}$$

$$A\left(\frac{x}{\epsilon}\right) \nabla u_\epsilon(x) = A^* \nabla_x u(x) + \tau\left(x, \frac{x}{\epsilon}\right) + s_\epsilon \quad \text{with} \quad \|s_\epsilon\|_{L^2(\Omega)} \leq C\epsilon^{1/2}$$

$$\int_{\Omega} A\left(\frac{x}{\epsilon}\right) \nabla u_\epsilon \cdot \nabla u_\epsilon dx = \int_{\Omega} A^* \nabla u \cdot \nabla u dx + o(1)$$

**Digression:** asymptotic expansions for the stress

We assume that

$$u_\epsilon(x) = \sum_{i=0}^{+\infty} \epsilon^i u_i \left( x, \frac{x}{\epsilon} \right), \quad \text{and} \quad \sigma_\epsilon(x) = A \left( \frac{x}{\epsilon} \right) \nabla u_\epsilon(x) = \sum_{i=0}^{+\infty} \epsilon^i \sigma_i \left( x, \frac{x}{\epsilon} \right),$$

with  $\sigma_i(x, y)$  function of the two variables  $x$  and  $y$ , **periodic in  $y$**  with period  $Y = (0, 1)^N$ . Plugging this series in the equation we find

$$-\operatorname{div}_y \sigma_0 = 0, \quad -\operatorname{div}_x \sigma_0 - \operatorname{div}_y \sigma_1 = f.$$

On the other hand,

$$\sigma_0(x, y) = A(y) (\nabla_x u(x) + \nabla_y u_1(x, y))$$

and

$$\sigma_0(x, y) = A^* \nabla_x u(x) + \tau(x, y) \quad \text{with} \quad \int_Y \tau \, dy = 0.$$

(One can prove that  $\tau$  is the solution of the dual cell problem.)



## Two-phase mixtures

We mix two isotropic constituents  $A(y) = \alpha\chi(y) + \beta(1 - \chi(y))$  with a characteristic function  $\chi(y) = 0$  or  $1$ .

Let  $\theta = \int_Y \chi(y) dy$  be the **volume fraction** of phase  $\alpha$  and  $(1 - \theta)$  that of phase  $\beta$ .

**Definition 7.6.** We define the set  $G_\theta$  of **all homogenized tensors**  $A^*$  obtained by homogenization of the two phases  $\alpha$  and  $\beta$  in proportions  $\theta$  and  $(1 - \theta)$ .

Of course, we have  $G_0 = \{\beta\}$  and  $G_1 = \{\alpha\}$ .

But usually,  $G_\theta$  is a **(very) large set of tensors** (corresponding to different choices of  $\chi(y)$ ).

### Non-periodic case

Homogenization works for non-periodic media too.

Let  $\chi_\epsilon(x)$  be a sequence of characteristic functions ( $\epsilon \neq$  period).

For  $A_\epsilon(x) = \alpha\chi_\epsilon(x) + \beta(1 - \chi_\epsilon(x))$  and  $f \in L^2(\Omega)$  we consider

$$\begin{cases} -\operatorname{div}(A_\epsilon(x)\nabla u_\epsilon) = f & \text{in } \Omega \\ u_\epsilon = 0 & \text{on } \partial\Omega. \end{cases}$$

**Theorem 7.7.** There exists a subsequence, a density  $0 \leq \theta(x) \leq 1$  and an homogenized tensor  $A^*(x)$  such that  $\chi_\epsilon$  converges “in average” (weakly) to  $\theta$ ,  $A_\epsilon$  **converges in the sense of homogenization** to  $A^*$ , i.e.,  $\forall f \in L^2(\Omega)$ ,  $u_\epsilon$  converges in  $L^2(\Omega)$  to the solution  $u$  of the homogenized problem

$$\begin{cases} -\operatorname{div}(A^*(x)\nabla u) = f & \text{in } \Omega \\ u = 0 & \text{on } \partial\Omega. \end{cases}$$

Furthermore, for any  $x \in \Omega$ ,  $A^*(x)$  belongs to the set  $G_{\theta(x)}$ , defined above.

**Disgression:** weak convergence or “in average”

Let  $\chi_\epsilon(x)$  be a sequence of characteristic functions,  $\chi_\epsilon \in L^\infty(\Omega; \{0, 1\})$ .

Let  $\theta(x)$  be a density,  $\theta \in L^\infty(\Omega; [0, 1])$ .

The sequence  $\chi_\epsilon$  is said to **weakly converge** to  $\theta$ , and we write  $\chi_\epsilon \rightharpoonup \theta$ , if

$$\lim_{\epsilon \rightarrow 0} \int_{\Omega} \chi_\epsilon(x) \phi(x) dx = \int_{\Omega} \theta(x) \phi(x) dx \quad \forall \phi \in C_c^\infty(\Omega).$$

**Lemma.** For any sequence  $\chi_\epsilon$  of characteristic functions, there exists a subsequence and a limit density  $\theta$  such that this subsequence weakly converges to this limit.

**Remark.** The space  $C_c^\infty(\Omega)$  can be replaced by  $L^1(\Omega)$  or any intermediate space of functions defined in  $\Omega$ .

## Application to shape optimization

Let  $\chi_\epsilon$  be a sequence (minimizing or not) of characteristic functions. We apply the preceding result

$$\chi_\epsilon(x) \rightharpoonup \theta(x) \quad A_\epsilon(x) \xrightarrow{\text{H}} A^*(x)$$

$$J(\chi_\epsilon) = \int_{\Omega} j(u_\epsilon) dx \rightarrow \int_{\Omega} j(u) dx = J(\theta, A^*),$$

with  $u$ , solution of the homogenized state equation

$$\begin{cases} -\operatorname{div}(A^* \nabla u) = f & \text{in } \Omega \\ u = 0 & \text{on } \partial\Omega. \end{cases}$$

In particular, the objective function is unchanged when:

$$J(\theta, A^*) = \int_{\Omega} f u dx, \quad \text{or} \quad J(\theta, A^*) = \int_{\Omega} |u - u_0|^2 dx.$$

## Homogenized formulation of shape optimization

We define the set of admissible **homogenized shapes**

$$\mathcal{U}_{ad}^* = \left\{ (\theta, A^*) \in L^\infty \left( \Omega; [0, 1] \times \mathbb{R}^{N^2} \right), A^*(x) \in G_{\theta(x)} \text{ in } \Omega, \int_{\Omega} \theta(x) dx = V_\alpha \right\}.$$

The **relaxed or homogenized** optimization problem is

$$\inf_{(\theta, A^*) \in \mathcal{U}_{ad}^*} J(\theta, A^*).$$

### Remarks

- ⇒  $\mathcal{U}_{ad} \subset \mathcal{U}_{ad}^*$  when  $\theta(x) = \chi(x) =$  or  $1$ .
- ⇒ We have enlarged the set of admissible shapes.
- ⇒ One can prove that the relaxed problem **always admit an optimal solution**.
- ⇒ We shall exhibit very efficient numerical algorithms for computing **homogenized optimal shapes**.
- ⇒ Homogenization **does not change the problem**: homogenized shapes are just the characterization of limits of sequences of classical shapes

$$\lim_{\epsilon \rightarrow 0} J \left( \chi \left( \frac{x}{\epsilon} \right) \right) = J(\theta, A^*).$$

- ⇒ We need to find an **explicit characterization** of the set  $G_\theta$ .

## Strategy of the course

The goal is to find the set  $G_\theta$  of all composite materials obtained by mixing  $\alpha$  and  $\beta$  in proportions  $\theta$  and  $(1 - \theta)$ .

- ⇒ One could do numerical optimization with respect to the geometry of the mixture  $\chi(y)$  in the unit cell.
- ⇒ We follow a different (and analytical) path.
- ⇒ **First**, we build a class of explicit composites (so-called sequential laminates) which will "fill" the set  $G_\theta$ .
- ⇒ **Second**, we prove "bounds" on  $A^*$  which prove that no composite can be outside our previous guess of  $G_\theta$ .

## 7.3 Composite materials

### Theoretical study of composite materials:

- ⇒ In dimension  $N = 1$ : explicit formula for  $A^*$ , the so-called **harmonic mean**.
- ⇒ In dimension  $N \geq 2$ , for two-phase mixtures: **explicit characterization of  $G_\theta$**  thanks to the variational principle of Hashin and Shtrikman.

### Underlying assumptions:

- ⇒ Linear model of conduction or membrane stiffness (it is more delicate for linearized elasticity and very few results are known in the non-linear case).
- ⇒ Perfect interfaces between the phases (continuity of both displacement and normal stress): no possible effects of delamination or debonding.



Dimension  $N = 1$ 

$$\text{Cell problem: } \begin{cases} -\left(A(y)(1+w'(y))\right)' = 0 & \text{in } [0, 1] \\ y \rightarrow w(y) & \text{1-periodic} \end{cases}$$

We explicitly compute the solution

$$w(y) = -y + \int_0^y \frac{C_1}{A(t)} dt + C_2 \quad \text{with} \quad C_1 = \left( \int_0^1 \frac{1}{A(y)} dy \right)^{-1},$$

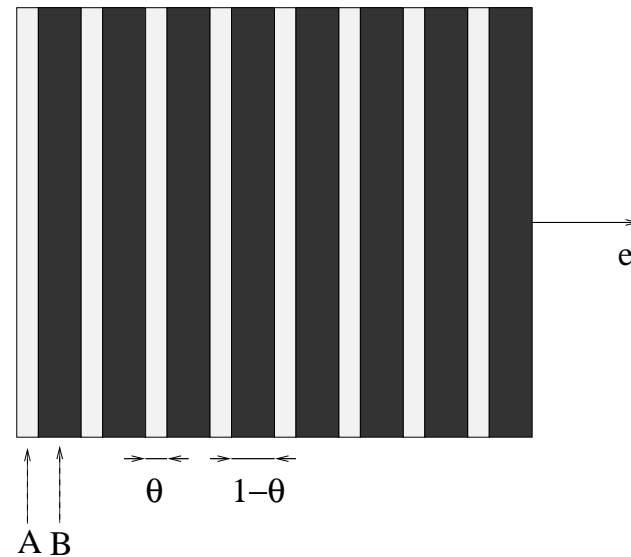
The formula for  $A^*$  is  $A^* = \int_0^1 A(y)(1+w'(y))^2 dy$ , which yields the **harmonic mean** of  $A(y)$

$$A^* = \left( \int_0^1 \frac{1}{A(y)} dy \right)^{-1}.$$

**Important particular case:**

$$A(y) = \alpha\chi(y) + \beta(1 - \chi(y)) \quad \Rightarrow \quad A^* = \left( \frac{\theta}{\alpha} + \frac{1 - \theta}{\beta} \right)^{-1}$$

## Simple laminated composites



In dimension  $N \geq 2$  we consider parallel layers of two isotropic phases  $\alpha$  and  $\beta$ , orthogonal to the direction  $e_1$

$$\chi(y_1) = \begin{cases} 1 & \text{if } 0 < y_1 < \theta \\ 0 & \text{if } \theta < y_1 < 1, \end{cases} \quad \text{with } \theta = \int_Y \chi \, dy.$$

We denote by  $A^*$  the homogenized tensor of  $A(y) = \alpha\chi(y_1) + \beta(1 - \chi(y_1))$ .

**Lemma 7.9.** Define  $\lambda_{\theta}^{-} = \left( \frac{\theta}{\alpha} + \frac{1-\theta}{\beta} \right)^{-1}$  and  $\lambda_{\theta}^{+} = \theta\alpha + (1-\theta)\beta$ . We have

$$A^* = \begin{pmatrix} \lambda_{\theta}^{-} & & & 0 \\ & \lambda_{\theta}^{+} & & \\ & & \ddots & \\ 0 & & & \lambda_{\theta}^{+} \end{pmatrix}$$

**Interpretation** (resistance = inverse of conductivity). Resistances, placed in series (in the direction  $e_1$ ), average arithmetically, while resistances, placed in parallel (in directions orthogonal to  $e_1$ ) average harmonically.

**Proof.** We explicitly compute the solutions  $(w_i)_{1 \leq i \leq N}$  of the cell problems.

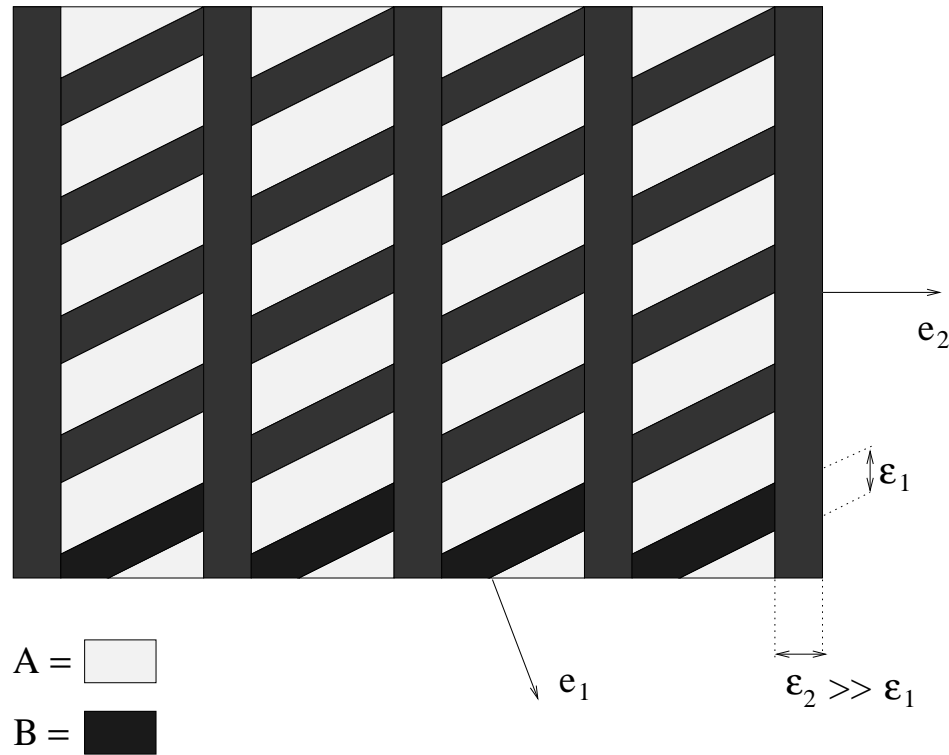
For  $i = 1$  we find  $w_1(y) = w(y_1)$  with  $w$  the **uni-dimensional** solution.

For  $2 \leq i \leq N$  we find that  $w_i(y) \equiv 0$  since, in the weak sense, we have

$$\operatorname{div}_y \left( \alpha \chi(y_1) e_i + \beta (1 - \chi(y_1)) e_i \right) = 0 \quad \text{in } Y,$$

because the normal component (to the interface) of the vector  $(\alpha \chi + \beta(1 - \chi))e_i$  is continuous (actually zero) through the interface between the two phases.

## Sequential laminated composites



We laminate again a laminated composite with one of the pure phases.

Simple laminate of two non-isotropic phases

**Lemma 7.11.** The homogenized tensor  $A^*$  of a simple laminate made of  $A$  and  $B$  in proportions  $\theta$  and  $(1 - \theta)$  in the direction  $e_1$  is

$$A^* = \theta A + (1 - \theta)B - \frac{\theta(1 - \theta) (A - B)e_1 \otimes (A - B)^t e_1}{(1 - \theta)Ae_1 \cdot e_1 + \theta Be_1 \cdot e_1}.$$

If we assume that  $(A - B)$  is invertible, then this formula is equivalent to

$$\theta (A^* - B)^{-1} = (A - B)^{-1} + \frac{(1 - \theta)}{Be_1 \cdot e_1} e_1 \otimes e_1$$

**Proof.** By definition

$$A_{ji}^* = \int_Y A(y) (e_i + \nabla_y w_i) \cdot e_j \, dy = \int_Y A(y) (e_i + \nabla_y w_i(y)) \cdot (e_j + \nabla_y w_j(y)) \, dy,$$

namely

$$A^* e_i = \int_Y A(y) (e_i + \nabla_y w_i) \, dy.$$

Consequently,  $\forall \xi \in \mathbb{R}^N$ , we have

$$A^* \xi = \int_Y A(y) (\xi + \nabla_y w_\xi) \, dy,$$

with  $w_\xi(y) = \sum_{i=1}^N \xi_i w_i(y)$  solution of

$$\begin{cases} -\operatorname{div}_y (A(y) (\xi + \nabla w_\xi(y))) = 0 & \text{in } Y \\ y \rightarrow w_\xi(y) & Y\text{-periodic.} \end{cases}$$

**Main idea:** defining  $u(y) = \xi \cdot y + w_\xi(y)$  we seek a solution, the gradient of which is constant in each phase

$$\nabla u(y) = a\chi(y_1) + b(1 - \chi(y_1)),$$

$$\Rightarrow u(y) = \chi(y_1)(c_a + a \cdot y) + (1 - \chi(y_1))(c_b + b \cdot y).$$

Let  $\Gamma$  be the interface between the two phases.

By continuity of  $u$  through  $\Gamma$

$$c_a + a \cdot y = c_b + b \cdot y$$

$$\Rightarrow (a - b) \cdot x = (a - b) \cdot y \quad \forall x, y \in \Gamma.$$

Since  $(x - y) \perp e_1$ , there exists  $t \in \mathbb{R}$  such that  $b - a = te_1$ .

By continuity of  $A\nabla u \cdot n$  through  $\Gamma$

$$Aa \cdot e_1 = Bb \cdot e_1.$$

(In particular, it implies  $-\operatorname{div}(A(y)\nabla u) = 0$  in the weak sense.)



We deduce the value of  $t = \frac{(A - B)a \cdot e_1}{Be_1 \cdot e_1}$ .

Since  $w_\xi$  is periodic, it satisfies  $\int_Y \nabla w_\xi dy = 0$ , thus

$$\int_Y \nabla u dy = \theta a + (1 - \theta)b = \xi.$$

With these two equations we can evaluate  $a$  and  $b$  in terms of  $\xi$ .

On the other hand, by definition of  $A^*$  we have

$$A^* \xi = \int_Y A(y) (\xi + \nabla w_\xi) dy = \int_Y A(y) \nabla u dy = \theta Aa + (1 - \theta)Bb.$$

An easy computation yields the desired formula

$$A^* \xi = \theta A\xi + (1 - \theta)B\xi - \frac{\theta(1 - \theta)(A - B)\xi \cdot e_1}{(1 - \theta)Ae_1 \cdot e_1 + \theta Be_1 \cdot e_1} (A - B)e_1$$

The other formula is a consequence of:  $M$  invertible implies

$$(M + c(Me) \otimes (M^t e))^{-1} = M^{-1} - \frac{c}{1 + c(Me \cdot e)} e \otimes e.$$

## Sequential lamination

We laminate again the preceding composite **with always the same phase  $B$** .

Recall that the homogenized tensor  $A_1^*$  of a simple laminate is

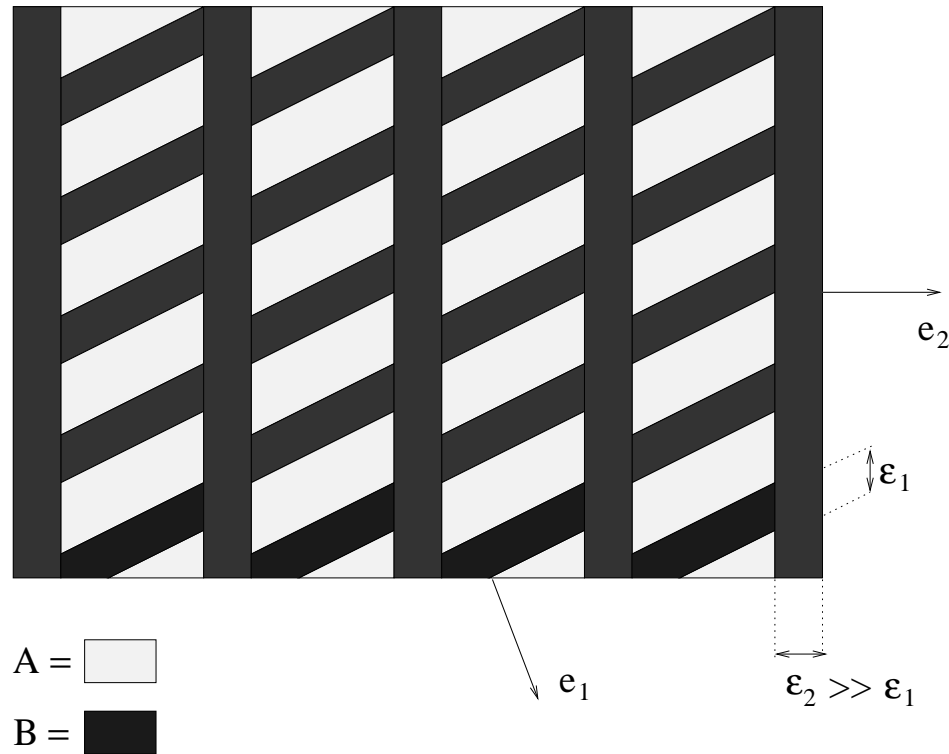
$$\theta (A_1^* - B)^{-1} = (A - B)^{-1} + (1 - \theta) \frac{e_1 \otimes e_1}{B e_1 \cdot e_1}.$$

**Lemma 7.14.** If we laminate  $p$  times with  $B$ , we obtain a **rank- $p$  sequential laminate with matrix  $B$  and inclusion  $A$ , in proportions  $(1 - \theta)$  and  $\theta$**

$$\theta (A_p^* - B)^{-1} = (A - B)^{-1} + (1 - \theta) \sum_{i=1}^p m_i \frac{e_i \otimes e_i}{B e_i \cdot e_i}.$$

with

$$\sum_{i=1}^p m_i = 1 \text{ and } m_i \geq 0, \quad 1 \leq i \leq p.$$



- ⇒  $A$  appears only at the first lamination: it is thus surrounded by  $B$ . In other words,  $A$  =inclusion and  $B$  = matrix.
- ⇒ The thickness scales of the layers are very different between two lamination steps.
- ⇒ Lamination parameters  $(m_i, e_i)$ .

**Proof.** By recursion we obtain  $A_p^*$  by laminating  $A_{p-1}^*$  and  $B$  in the direction  $e_p$  and in proportions  $\theta_p$ ,  $(1 - \theta_p)$ , respectively

$$\theta_p (A_p^* - B)^{-1} = (A_{p-1}^* - B)^{-1} + (1 - \theta_p) \frac{e_p \otimes e_p}{B e_p \cdot e_p}.$$

Replacing  $(A_{p-1}^* - B)^{-1}$  in this formula by the similar formula defining  $(A_{p-2}^* - B)^{-1}$ , and so on, we obtain

$$\left( \prod_{j=1}^p \theta_j \right) (A_p^* - B)^{-1} = (A - B)^{-1} + \sum_{i=1}^p \left( (1 - \theta_i) \prod_{j=1}^{i-1} \theta_j \right) \frac{e_i \otimes e_i}{B e_i \cdot e_i}.$$

We make the change of variables

$$(1 - \theta) m_i = (1 - \theta_i) \prod_{j=1}^{i-1} \theta_j \quad 1 \leq i \leq p$$

which is indeed one-to-one with the constraints on the  $m_i$ 's and the  $\theta_i$ 's ( $\theta = \prod_{i=1}^p \theta_i$ ).

The same can be done when exchanging the roles of  $A$  and  $B$ .

**Lemma 7.15.** A rank- $p$  sequential laminate with matrix  $A$  and inclusion  $B$ , in proportions  $\theta$  and  $(1 - \theta)$ , is defined by

$$(1 - \theta) (A_p^* - A)^{-1} = (B - A)^{-1} + \theta \sum_{i=1}^p m_i \frac{e_i \otimes e_i}{Ae_i \cdot e_i}.$$

with

$$\sum_{i=1}^p m_i = 1 \text{ and } m_i \geq 0, \quad 1 \leq i \leq p.$$

**Remark.** Sequential laminates form a very rich and **explicit** class of composite materials which, as we shall see, describe completely the **boundaries of the set  $G_\theta$** .