# **GP-Based Motion Control Design for the Double-Integrator System Subject to Velocity Constraint**

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#### ABSTRACT

The motion control problem for the double-integrator system subject to velocity constraint is addressed. A novel methodology, which consists of a two-stage process and regards a trade-off between natural and learned behaviors to develop a family of analytic controllers, is proposed. To this end, firstly, a natural behavior is designed to achieve asymptotic tracking of a desired continuous trajectory by using a Control-Theory approach. Secondly, learned behaviors are discovered by using a Genetic Programming approach to synthesize an analytic controller to ensure a bounded velocity of the system. The integration of these approaches allows the system to exhibit a good tracking performance while keeping the velocity bounded to a desired value, freely set by the user. Simulation results are provided to illustrate the effectiveness of the proposal, and a comparison with a traditional *Control-Theory-Based* solution is also given and discussed.

### **KEYWORDS**

Motion control design, genetic programming, double-integrator system, bounded velocity

#### ACM Reference format:

Ollin Peñaloza-Mejía, Eddie Clemente, Marlen Meza-Sánchez, Cynthia B. Pérez, and Francisco Chávez. 2017. GP-Based Motion Control Design for the Double-Integrator System Subject to Velocity Constraint. In *Proceedings* of *GECCO '17 Companion, Berlin, Germany, July 15-19, 2017, 2* pages. DOI: http://dx.doi.org/10.1145/3067695.3076094

## **1** INTRODUCTION

The double-integrator system is one of the most fundamental plants used in control theory due to its wide applications in engineering (see e.g. [1, 2]). Its dynamics is described by the second-order differential equation

$$\ddot{q}(t) = u(t),\tag{1}$$

GECCO '17 Companion, Berlin, Germany

where  $q(t), \dot{q}(t), \ddot{q}(t) \in \mathbb{R}$  is the position, velocity and acceleration, respectively, and  $u(t) \in \mathbb{R}$  is the control input to be designed to impose a desired behavior. The dynamics (1) describes the motion of a single-degree-of-freedom rigid body with unit moment of inertia and simplified models of mechanical systems, commonly used in Robotics and other fields (see e.g. [3-5]). The motion control problem for this system include asymptotic convergence to a given reference. Though this problem has been solved from the control theory approach, the input and the velocity, in general, can take any value, which in practice could remain saturated because the systems have physic limits. However, the operation of systems under saturated conditions for long periods of time has proved to cause damage of parts, deterioration of performance, and even instability. In this work, the integration of both, Control Theory (CT) and Genetic Programming (GP) approaches, is proposed to build up a family of controllers valid for the double-integrator system, to achieve asymptotic tracking of a desired continuous trajectory while bounding the system velocity (to a desired value). The main contributions of this paper are summarized as follows.

- A methodology for learning analytic control functions based on genetic programming.
- A *natural behavior* is generated for a double-integrator system by means of a classical CT-based controller. Next, such behavior is complemented, by implementing a GP approach, upon that the system *learns* how-to accomplish a previously established performance considering velocity constraints.

Then, our control objective is described as the design of the control input u(t) such that the following two performance conditions are achieved. First, the position q(t) asymptotically converges to a desired trajectory  $q_d(t)$ ; that is

$$\lim_{t \to \infty} \left( q_d(t) - q(t) \right) = 0. \tag{2}$$

Second, the velocity  $\dot{q}(t)$  remains within a boundary layer defined by the desired velocity bound  $\dot{q}_{max}$ ; that is

$$|\dot{q}(t)| \le \dot{q}_{max}, \quad \forall \quad t \ge 0.$$
(3)

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Table 1: Some solutions discovered by the evolutionary process and control laws used for performance comparison.

Solution	Mathematical expression		Fitness
$u_{GP_1}$	$10 * (\dot{q}_d(t) - \dot{q}(t)) + sinh(sinh(3 * (\dot{q}_d(t) - \dot{q}(t))))$		0.94
$u_{GP_2}$	$\boxed{2 * \dot{q}_d(t) - \dot{q}(t) + \sinh(3 * (tanh(\dot{q}_d(t) - \dot{q}(t)) - \dot{q}(t)) + \dot{q}_d(t)) - tanh(tanh(\dot{q}_d(t) - \dot{q}(t))) + tanh(\dot{q}_d(t) - 2 * \dot{q}(t)) - \dot{q}(t))} + tanh(\dot{q}_d(t) - 2 * \dot{q}(t)) - \dot{q}(t) + tanh(\dot{q}_d(t) - \dot{q}(t)) + tanh(\dot{q}_d(t) - 2 * \dot{q}(t)) - \dot{q}(t) + tanh(\dot{q}_d(t) - \dot{q}(t)) + tanh(\dot{q}_d(t) - 2 * \dot{q}(t)) - \dot{q}(t) + tanh(\dot{q}_d(t) - \dot{q}(t)) + tanh(\dot{q}_d(t) - $		0.92
	$tanh(2*\dot{q}_d(t)-\dot{q}(t))$		
$u_{GP_3}$	$ \begin{array}{l} (\min(sech(sech(vmax)) - 2 * \dot{q}_d(t) + 3 * \dot{q}(t), asin(\epsilon)))^2 - \dot{q}(t) + \dot{q}_d(t) + tanh(\min(tanh(\dot{q}_d(t) - \dot{q}_d(t)), \dot{q}(t))) - min(tanh(\dot{q}(t) - \dot{q}_d(t)), asin(\epsilon)) - 2 * (\dot{q}(t) + \dot{q}_d(t)) + cosh((\min(\dot{q}(t) - asin(\epsilon), asin(min(tanh(\dot{q}(t) - \dot{q}_d(t)), \dot{q}_{max})) - sech(\dot{q}(t) - \dot{q}_d(t))))^2) - tanh(\dot{q}_{max} - \dot{q}_d(t) + \dot{q}(t)) \end{array} $		0.89
$u_{ ext{tanh}}$	$(\tanh((\dot{q}(t) + \dot{q}_{max})/\Delta))/2 - (\tanh((\dot{q}(t) - \dot{q}_{max})/\Delta))/2$		2989.68
u <sub>pcf</sub>	1, 0	$\dot{q}(t) < \dot{q}_{max}$	
	$(1 - \cos((\pi/\Delta) * (\dot{q}(t) - \dot{q}_{max})))/2,$	$-\dot{q}_{max} \leq \dot{q}(t) < -\dot{q}_{max} + \Delta$	
	0, -	$-\dot{q}_{max} + \Delta \le \dot{q}(t) \le \dot{q}_{max} - \Delta$	0.96
	$(-1 + \cos((\pi/\Delta) * (\dot{q}(t) + \dot{q}_{max})))/2,$	$\dot{q}_{max} - \Delta < \dot{q}(t) \le \dot{q}_{max}$	
	-1, 0	$\dot{q}(t) > \dot{q}_{max}$	

### 2 SYNTHESIS OF TRACKING CONTROLLERS

The proposed control input for the double-integrator system is a combination of two controllers given by

$$u(t) = u_{CT} + u_{GP},\tag{4}$$

where  $u_{CT}$  is a traditional PD-like controller used to achieve asymptotic tracking of the reference and  $u_{GP}$  is used to keep the velocity within the desired limits. The design of  $u_{GP}$  is not evident and is a real challenge since there is no established procedure to propose such analytic controller. An alternative approach is then proposed for designing  $u_{GP}$  by using Genetic Programming, in which the system stability, the tracking performance and the maximal allowed velocity can be considered simultaneously. Thus, the fitness function is defined in (5), including the Root Mean Square Error (RMSE) between the position error and the velocity error, the parameter  $N_{oc}$  which takes into account the number of milliseconds where boundary limits are exceeded by the controlled system, and the initial conditions q(0) and  $\dot{q}(0)$ . Thus, the fitness function is defined as the average performance of a set of M initial conditions

$$f = \frac{\sum_{i=1}^{M} \left( \sqrt{\frac{\sum_{t=0}^{n} (q_d(t) - q(t))^2}{n}} + \sqrt{\frac{\sum_{t=0}^{n} (\dot{q}_d(t) - \dot{q}(t))^2}{n}} + N_{oc} \right)_i}{M} \quad (5)$$

#### **3 SIMULATION RESULTS**

Some discovered fittest solutions  $u_{GP_i}$ , i = 1, 2, 3 as well as stateof-the-art proposals  $u_{tanh}$  and  $u_{pcf}$ , are shown in Table 1. A performance comparison against our fittest solution using the same parameters and initial conditions is shown in Figure 1.

#### 4 CONCLUSIONS

A new methodology towards the development of controllers merging CT and GP approaches was proposed. It was applied to solve the motion control problem for the double-integrator system subject to velocity constraints. The proposal allows the system to achieve asymptotic tracking of a given reference while bounding the velocity to a desired value. The family of controllers found by the evolutionary process are fittest, compared to solely Control-Theory-based solutions, under the same settings. Future work will extend the proposed framework to improve performance of the controlled system applying a Multi-Objective Genetic-Programming-based approach considering physical constraints of other variables (e.g. torques

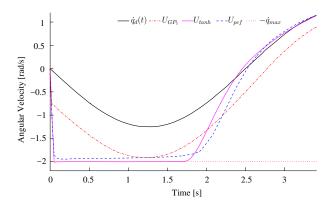


Figure 1: Detailed comparison of exhibited velocity with the different approaches during the settling time.

and/or displacements) to increase feasibility of real-world implementations and to facilitate the stability analysis of the closed-loop system.

# ACKNOWLEDGEMENTS

This work was supported by ITSON, TecNM project 5748.16-P, CONACYT Cátedras 2459, Spanish Ministry of Economy, Project UEX:EPHEMEC (TIN2014-56494-C4-2-P); Junta de Extremadura, and FEDER, project GR15068 and GR15130.

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